NPP Operational History and the Uncertainties of Radionuclides Relevant for the Final Disposal of PWR Spent Fuel – 15149 🏾 🍼 JÜLICH

INTRODUCTION A requisite for the official approval of the safe final disposal of SNF is a comprehensive specification and declaration of the nucle- RADIONUCLIDES - RESULTS ar inventory in SNF by the waste supplier. In the verification process both the values of the radionuclide (RN) activities and their uncertainties are required. Burn-up calculations based on typical and generic reactor operational parameters do not encompass any possible uncertainties observed in real reactor operations. At the same time, the details of the irradiation history are often not well known, which complicates the assessment of declared RN inventories. Here, we have compiled a set of burn-up calculations accounting for the operational history of 339 published or anonymized real PWR fuel assemblies. These histories were used as a basis for a "SRP analysis", to provide information about the range of the values of the associated secondary reactor parameters (SRP's). Hence, we can cal- DOWNTIME ANALYSIS culate the realistic variation or spectrum of RN inventories. SCALE 6.1 model description: has been employed for the burn-up calculations. The results have Geometry: FA 16×16 AFA 3G Burn-up: 65 GWd/tHM been validated using experimental data from the online database – 36 MW/tHM SFCOMPO-1 and -2 [3],[4]. 4.0 % wt U-235 900 K

580 K

10.408 g/cm_n

0.73 g/cm_g

460 ppm

6 Cycles with DT 0, 50, 75, 100, 400 c

Downtime 50 d

Downtime 75 d

Downtime 100 d
 Downtime 400 d

Am-241 by CT 0

_ 25 _ _ _ Downtime 0

---- Downtime 50 d

Downtime 75 d

----- Downtime 100 d

Downtime 400 d

SECONDARY REACTOR PARAMETER's (SRP) -

parameters of a PWR operational history:

- Specific Power (SP)
- Downtime (DT)
- Initial Enrichment (IE) Fuel Density (FD)
- Fuel Temperature (FT)
- Moderator Density (MD)
- Moderator Temperature (MT) Boric Acid concentration (BA)
 Analysis for





Table I RN relevant for the final disposal of PWR spent fuel



RN name	<mark>Cs-134</mark>	Eu-154 P	⁹ u-241 Sm	- <mark>151</mark> Am-24	<mark>3</mark> Cm-244	Cm-245 Cm	1-246 Cm·	-247 Cs-135	Pu-240	U-235 <mark>Am-</mark> 2	241 Am-242	m Ce-144	Cm-242 Ca	s-137 <mark>Pu-2</mark>	. <mark>38</mark> Ru-106	5 Sb-125 <mark>S</mark>	Sr-90 <mark>U-23</mark>	2 U-234 Np-	237 Pu-2	239 Pu-24	2 Se-79	Sn-126 Tc-	<mark>-99</mark> U-238	8 Ac-227 <mark>A</mark>	Ag-108m Ag	g-110m <mark>C-14</mark>	4 Cf-249 C	Cf-251 Cm-2	243 Cm-2	-248 Eu-152	Eu-155 H-3	3 1-129 K r	r-85 Mo	<mark>-93</mark> Nb-94 Nb	-95 Pa-2	231 Pd-107 P	<mark>m-147</mark> Pr	-144 Pu-243	Pu-244 Ra	<mark>a-226</mark> Rh-1	06 Ru-103	Sb-124 Th-	-229 Th-231	0 Th-232	<mark>U-233</mark> U-23	3 <mark>Y-90</mark> Zr	-93 Zr-95	Cf-252 Ca-4	1 CI-36 Co-58	3 Co-60 Fe	e-55 Mn-54	Ni-59 Ni-63
RN list for long-term safety [1	1] x	X	X X	(X	Х	X	Х	Х	X	X X	X	X		X X	X	X	X X	X	X X	Х	Х	X	X X	X		X		Х	Х	X		X		X X	X	X		X	X	X X			X X	X	X X	X	X	X	X	X		XX
CSD-C ¹ list	Х	X	X X	(Х	Х	X	X	x x	X	X X	X	X	X	X X	X	X	X X	X	X X	Х	Х	X	X X	X	Х	X X	X	X X	Х	X X	X X	X	X	X X	X X	Х	Х	X X	X	X X	X	X	X X	X	X X	X	X X	X X	X X	X	X X	XX
Calculated data (only fuel)	X	X	X X	(X	Х	X	X	x x	X	X X	Х	X	X	x x	X	X	X X	X	x x	Х	X	X	x x	X	Х	x x	X	X X	Х	x x	X X	X	X	x x	x x	X	X	x x	X	X X	X	X	x x	X	x x	X	X X					
Measured data [3], [4]	Х	X	X X	(X	Х	X	X	x x	X	X X	Х	X	X	X X	X	X	X X	X	X X	Х	Х	X	X X																													
100% agreement calc-vs-mea	as x ²	χ ²	χ ² >	(X	Х	X	X	X X	X	X																																										
CT correction required	Х	X	Х		Х					X	X	X	X	X	X	X	X X	X						X		X		Х		X	X X		X		X		X	X		X X	X	X	X	X	X	X	Х					
			<u>,</u>	<u>г.</u> рт	 							I															L									· · ·			•					· ·	•		I	μ				

1: Lolis Standard de Déchets Compactés [2], 2: 100% agreement calc-vs-meas after C1 correctio

<u>Ivan Fast,</u> Yuliya Aksyutina, Holger Tietze-Jaensch and Dirk Bosbach Institute of Energy- and Climate Research, Nuclear Waste Management and Reactor Safety Research, IEK-6, Forschungszentrum Jülich GmbH, Germany, i<u>fast@fz-juelich.de</u>



or cooling time (CT) 0, 1, 3, 5 y Figure II. Downtime (DT) vs. number of fuel assemblies





Figure V. Calculated vs. measured data from SFCNMPN-1131 100 % anreement



- Experimentally underpinned operation history FA data are often incomplete (especially for cycle values of MD, MT, FD, FT, BA).
- There is a linear correlation between BU and IE. SP, MD, MT.
- There is a very good agreement with the theoretical data for MD vs MT.
- It is feasible to determine SRP limits.
- For most fission products operational history without DT is conservative.
- The activity of most actinides in the case of operational history without DT is either independent of DT (e.g. U-235, U-238, Pu-239, Np-237) or underestimated. However, the strongest influence of DT decreases with increasing CT.
- DT analysis enables calculations with DT=0.
- The RN behavior by variation of SRP's can be generally divided in four subgroups (s. Table I):
- Independent of all SRP:
- Dependent of all SRP:
- Strongly dependent of IE:
- Strongly dependent of IE and SP: blue Unmarked RN's are absent in the fuel (e.g. activation product in cladding).
- Preliminary comparison of calc. and meas. data reveals very good agreement. However, for some cases corrections are required.

OPEN QUESTIONS

- Explanation deviations of calculated vs. measured data (e.g. Am-241 factor 4, U-234 factor 10)
- Validation of RN's for which the measured data are not available







Figure VII. Calc. vs. meas. from SFCOMPO-1 (3), CT co



Figure VI. Calc. vs. meas. from SFCOMPO-1 [3], 100 % agreement after CT correction Figure VIII. Calc. vs. meas. from SFCOMPO-2 [4], with meas. uncertainties

OUTLOOK

- Include the measured data from SFCOMPO-2 (4), which contains high burn-up data and meas. uncertainties
- Find an explanation for the poor agreement between calculated and measured data
- Correcting measured data on downtime
- Determine the bandwidth of the nuclides for which measured data are not available
- Further analysis of the results for different scenarios in case if operational history not completely available

REFERENCES

A. Meleshyn, U. Noseck, "Radionuclide Inventory of Vitrified Waste after Spent Nuclear Fuel Reprocessing at La Haque", Geselschaft für Anlagen- und Reaktorsicherheit (GRS) mbH, GRS-294, September 2012

°2] B. Kienzler, A. Loida, "Endlagerrelevante Eigenschaften von hochraiodaktiven Abfallorodukten". Forschunoszentru Karlruhe GmbH, FZKA 6651, 2001

[3] Nuclear Energy Agency NEA/DECD, SFCOMPO-1 database, http://www.oecd-nea.org/sfcompo/Ver.2/Eng /, 2015 [4] NEA-DECD, SFCOMPD-2 database, https://www.oecd-nea.org/science/wpncs/ADSNF/, 2015

ACKNOWLEDGMENT

- Wissenschaftlich Technische Ingenieurberatung GmbH (WTI) for providing of the anonymized FA data
- NEA-DECD for providing of the access to SFCOMPO-2 database
 NEA-DECD for providing of the access to SFCOMPO-2 database

				с ÷.			
Π		Π	С.	tı.	Π		
		Γ.	Ι.				
	•					• •	•